



This article is for those who want to make their own car amplifier. The basics of calculation will be discussed below. If you have understood it, you will be able to make a car amplifier yourself.

THE DESIGN OF CAR POWER AMPLIFIER

There are many designs of good amplifiers published, solid state (SS) or tube designs. But few have written the design of a car power amplifier. Actually, the difficulty of designing the car power amplifier does not lie with the audio power amplifier, but it is more about providing the switching power supply. As we know, the output power of any audio power amplifier is approached by the formula:

$$P = V_{pp}^2 / (8 \cdot R_L)$$

where V_{pp} = peak to peak supply voltage, R_L is the speaker impedance load. For a car voltage of 12Vdc, if we connect it to 4 Ohm speakers, we will only have a power of $144/32 = 4,5$ Watt. Bridging the amplifier will double the power, but will never be more than 40 W.

If we want to make a more powerful amplifier, let's say 170 watt at 4 ohm speaker load, we will need a supply voltage of 74Vpp, or +/- 37 Vdc. The way to have this voltage from a car supply of 12VDC is to make a DC-DC converter.

In this article, I will discuss the car power amplifier in 3 steps:

1. The design of an audio power amplifier
2. The design of a DC-DC converter
3. Miscellaneous tips for making a car power amplifier.

1. THE DESIGN OF AUDIO POWER AMPLIFIER

In [fig1](#) we can see that an audio power amplifier can be split into 3 main functions, that is:

- First stage / input stage
- Second stage / voltage amplifier stage
- Third stage / output stage

First stage is the stage that receives the input audio signal and Negative Feedback (NFB) signal from the output of the amp. Feedback is the back signal used to stabilize the audio amplifier, like the gain factor. For the first stage built by discrete transistors, both signals are fed to the base of the transistor, like in [fig1](#). Both bases of the transistors are the Non-Inverting input and Inverting Input, like those in the op-amp.

Second stage is the stage that is responsible for the Voltage Gain in the power amplifier.

Third stage is the Current Gain.

We can explain those stages in a **simple way** like this: Input signal, like from a car radio or CD player, has a low voltage, about 1Vpp with a few milliampere current. To produce a power of 170 Watt at 4 ohm speaker load, the signal has to have a magnitude of 28Vpp and a current of 6.5A (from the equation of $P = I^2 \cdot R = V^2 / R$)

The first stage receives this signal in the non-inverting input and the inverting input receives NFB signal to make sure the voltage gain that the amplifier produces has a constant number, let's say 28 x. The output signal from the first stage has not reached 28Vpp, it tends to have a magnitude similar to the input voltage. The second stage amplifies the voltage that the first stage generates. The second stage will amplify the voltage to produce a signal that is 28x larger for the amplifier to have a 28Vpp signal from a 1Vpp signal, but this 28Vpp signal still has a small current, only a few mA and cannot drive the speaker load. The third stage amplifies the current from a few mA to 6.5 A.

Of course, the explanation for the three stages above is not that simple in the real amplifier. We should take the nature's law for a transistor gain, that is $G = R_C / R_E$. This principle must be applied in each transistor in those 3 amplifier stages.

FIRST STAGE

First stage designs have a main component, that is Constant Current Source (CCS) which can be seen in [fig2](#)

. One of the basic electronic laws that works on every circuit is that the voltage drop of the Base and Emitter (V_{be}) equals the drop voltage of one diode = 0.67V. It can be seen in [fig2](#) that the voltage drop of 2 diodes IN4148 = $2 \times 0.67V = 1,34V$. We can see in R_E and Q_1 , then $V = 0,67$ is subtracted by V_{be} of Q_1 and the other 0,67V will be the drop of R_E . So we will have a Constant Current Source of $0,67 / R_E$. In [fig2](#) the I_C is = 4,4mA. CCS first stage varies between 1-4mA.

In [fig1](#) first stage, each component will be explained like this:

- R_1 is the impedance of the audio amplifier, the range is 10 Kohm - 47Kohm
- C_1 is the highpass filter from the equation: $f_{hp} = 1 / (2 \times \pi \times R_1 \times C_1)$
- R_{E1} and R_{E2} is between 50-150 ohm
- R_{M1} and R_{M2} is picked up so the voltage drop will be 50mV - 150mV
- Q_3 and Q_4 is the Current Mirror that ensures the current in R_{M1} and R_{M2} will have the same magnitude.
- R_F and C_F will be discussed later.

Before we discuss Second Stage and Third stage, first we will discuss the amplifying effect of a transistor. In [fig3a](#) we will see a circuit of Common Emitter Mode (CEM). This circuit will amplify the voltage. In [fig3b](#) we see a Common Collector Mode (CCM). This circuit is the current amplifier without voltage amplifier. So if we want to amplify voltage we use CEM circuit and to amplify current we use CCM circuit.

SECOND STAGE

The Second stage responsible for all voltage gain (Maximum Voltage Swing) in an audio power amplifier. This is why the Second stage is generally known as VAS or Voltage Amplifier Stage. This stage consists of a voltage amplifier/CEM transistor (Q5 in [fig1](#)) in the bottom, Constant Current Source in the top, and a bias control circuit in the middle. Second stage CCS has current magnitude between 4-8mA

In the second stage there is an important capacitor for an audio power amplifier, that is Miller Capacitor (CC in [fig1](#)). CC defines the pole of the frequency response for an audio amplifier and the magnitude usually in small order (several pF).

Bias control circuit consists of a transistor, resistor and a VR like in [fig5](#). This circuit uses a transistor that is placed in the heatsink, because the transistor has good heat compensation factor (for bipolar transistors). For the amplifier that uses MOSFET transistor for the final device, the bias circuit only needs a potentiometer or diode only because MOSFETs have different heat characteristics than bipolar transistors. The bias voltage magnitude depends on the type of the third stage used, which will be discussed later.

THIRD STAGE

Third stage / Output Stage is the current amplifier. Third stage and the bias circuit will define whether an amplifier works in class A, class AB or class B.

It can be said that almost 90% of car audio power amplifier works in class B. Operation in class B does not mean that the sound produced is not good or corrupted. With good design, we will have good audio results, both from class A or class B. The choice of class B in car audio power amplifier is connected to efficiency and the heat generated. Heat generated is a very important factor, because if not considered carefully, it will lead to amplifier breakdown.

Many configurations of the output stage can be seen in [fig4](#). Each configuration has different optimum bias voltage. It depends on how many V_{be} 's that have to be passed. Example: In [fig4\(a\)](#) the signal has to pass 4 V_{be} 's, which is V_{be} Q1, Q3, Q4 and Q2. So the optimum bias = $4 \times 0.67V = 2.8V$.

Both 3 stages that we have discussed above, if we connect them together will be a circuit that can be seen in [fig5](#). Parts of this circuit can be explained like this:

- The value of Negative Feedback (NFB) resistor is determined by determining the gain factor with the equation: $Gain = 1 + (R10/R8) = 1 + 10k/500 = 21$. The value of R10 = value of R1 to balance input. R20 and C7 are the pole and slope compensator.
- C2 limits the DC gain factor, value ranging from 47-220 μF , usually using a nonpolar capacitor.
- R21, R22 and C11 will stabilize CCS. Here we use CCS with 2 transistor system, but the equation used is still the same, that is $I_c = 0.67/RE$.
- The output of differential pair is tapped from collector of T10 and sent to VAS which is built by T12 and T4. This configuration is called Darlington VAS and the value of R8 is standard.
- C3 is the Miller capacitor with a value of 100pF.
- C5 is called Speed Up Capacitor. Several designs do not use this capacitor.
- R18, C6, L1 and R19 are output power stabilizers. If there is any oscillation occur in the audio power amplifier, the first to be effected is R18 besides the final transistors.

Car Power amplifier usually loaded by low impedance speakers, usually 4 ohms and can reach $\frac{1}{2}$ ohm on bridge mode. Here we know the term "High Current Amplifier". The difference is the number of final transistors, or in [fig5](#) it is the number of pairs of T7 and T8. As a rule of thumb, the number of transistor needed first has to be calculated by equations above, and then we determine the number of final transistor needed with assumption that 1 transistor can handle 50 Watt output. A pair of bipolar transistor can handle 100 Watt. The power is raised by paralleling several output transistors, so the current flowing will be larger. For large number of final transistors, we change the predriver stage with darlington configuration.

Several designs use symmetrical design, like those used in AXL and Crescendo schematic. This design is developed from the basic principle above, but the signal handling for + and - part is handled by complementary circuits.

I have an example about another kind of power amplifier, that is a non-feedback amplifier. You can view the principles of the "millennium power amplifier" in the www.lcaudio.com. This amplifier has a certain gain factor in first and second stage, while the third stage is only current amplifier.

2. THE DESIGN OF DC-DC CONVERTER

For building car power amplifier, we need symmetrical power supply (+, 0, -) by building DC-DC converter. The converter system discussed below will be the SMPS (Switch Mode Power Supply) type PWM (Pulse Width Modulation). This system will deliver stable output voltage, regardless of the input voltage (usually the car electrical system will range in 9-15Vdc).

To explain the SMPS type PWM, it can be analogized by the next example. Look at [fig6](#). There is a voltage pulse V1 on-off with 50% width. These pulses if passed through suitable L and C filter will be transformed into straight voltage of V2 which is $V2 = \frac{1}{2} V1$. (noticed the marked area below pulsed V1 is the same total area of the marked straight V2). With the same logic, if the pulse width of V1 is narrowed, we will have a lower V2 and if we enlarge the width of V1 pulse, we will have higher V2. Some may ask, how can we get 30VDC from the car's 12VDC? The answer is simple. If we get the V1 voltage to 60VDC, then in the 50% duty cycle, we will get 30VDC straight. This is the part where the power switching transformer takes control, to make the 60VDC from 12VDC, and then chopped by the PWM. This is the principle of PWM. (Like the principle of class D digital power amplifier). In this design, we use regulating PWM IC's, like TL494, TL594, SG3524, SG3525. These IC's will compare the output of DC-DC converter with a reference voltage. If the output of DC-DC converter is smaller than reference voltage, then the IC will enlarge the pulse width so the voltage will raise equally to reach determined voltage. So as if the output of DC-DC converter is higher than the reference voltage, the IC will narrow the pulse width so the output voltage will be lowered to the determined voltage.

Generally SMPS used in car audio amplifier is the push-pull system with switching frequency between 20-70Khz. In push pull system like in [fig7](#), Q1 and Q2 gives alternating switched current pulses so the transformer will be objected to maximum flux swing change without saturating the core.

In this design we will use PWM IC with SG3524 from SGS Thompson. Specifications can be seen in SGS Thompson's website. [Fig8](#) shows the configuration of 16 pins on this IC. To make it simpler, let's design a SMPS by explaining the function of each pin.

For the stereo power amplifier in [fig5](#), we will need a SMPS 12Vdc input and symmetrical output of +/- 37Vdc with 8A rating.

1. First we make the Remote Turn On circuit, which is connected from the car radio / CD player. The circuit can be seen in [fig9a](#). This circuit will turn on the SMPS by giving 12Vdc to pin 12, pin 13 and pin 15.
2. The SMPS switching frequency is determined 50Khz. For this, the clock inside IC SG3524 is adjusted $2 \times 50 \text{ KHz} = 100\text{KHz}$. This clock is built up by pin 7(Ct) and pin 6(Rt). The approach can be done with equation $F_{clk} = 1 / (Rt \times Ct)$. Here we use $Ct = 1\text{nF}$ and $Rt = 10\text{Kohm}$ like in [fig9b](#)
3. Pin 2(Non Inv In). In pin 2 we put stable reference output for the SMPS. Here we use reference voltage of $\frac{1}{2}$ from reference pin 16.
4. Pin 1(Inv In) is the output voltage detector. Pin 1 is connected to the optoisolator type 4N35 like in [fig9b](#). Optoisolator is an important component in making this SMPS so we can have Floating Secondary Ground which will prevent noises (especially whine/storing) if the power amplifier is placed in car. The value of zener diode is $2 \times 37\text{V} = 74\text{V}$. If it is difficult to have zener voltage of 74 V, then we can series several zener values until we have total of 74 V.
5. Pin (4) and pin(5) are not used and connected to ground, pin(8) and pin(10) connected directly with ground.
6. Pin no 9(Comp) determines slope and pole of feedback from the whole SMPS system. In this design we use only 1 capacitor of 100nF.
7. Pin no 16(Vref) gives reference voltage of 5,1 Vdc. This pin is placed with 10nF as a voltage stabilisator.
8. The output ripple (Vr) of the SMPS is determined by equation :

$V_r = 8 \times 10^{-6} \times I / C_o$. With $I = 8\text{A}$ and $V_r = 0,029\text{V}$ we will have C_o of 2.200uF in +37Vdc ->-37Vdc rail or 4400uF each in +37Vdc_0 and 4.400uF in 0_-37Vdc.

9. For output filter capacitor of 2.200uF, we will need approximately $4 \times 2.200\text{uF}$ or 8.800uF in the SMPS's input 12Vdc. The larger the value of this capacitor, more energy stored for the SMPS.
10. Output filter inductor L_o is determined by : $L_o = 0,5 \times V_{out} / (I \times F)$. With $V_{out} = 2 \times 37\text{V} = 74\text{V}$, $I = 8\text{A}$ dan $F = 50\text{KHz}$, we will have $L_o = 0,092\text{mH}$ or $L_o = 0,046\text{mH}$ on each supply rail + and - 37Vdc.
11. Pin 11 and pin 14 are output pins that will drive the primary winding switching mosfets. Inside IC SG3524 both pins have already operated in mode push-pull. The circuit for driving power mosfets can be seen in [fig9b](#). The number of power mosfet used is 3 in each transformer primary. So total there is 6 power mosfets type BUZ11.
12. Transformer(trafo) for SMPS is selfwound from ferrite toroidal core (like donuts) like in [fig10](#). It is very important that for SMPS frequency above 20Khz, we cannot use iron core transformer like we use in homes. The ferrite core transformer will have black color like in the speaker magnets, but do not have magnetizing force. The basic of equation for switching power supply with 12Vdc input is:

(1) $N_p = 1,37 \times 10^5 / (F \times A_e)$, where N_p = primary number of turns, F = switching frequency, $A_e = X \times Y$ = window area of ferrite in cm^2 . Look at [fig10](#). To make it easy to wound the transformer, we will have to choose the toroid core with minimal diameter of 2,5 cm and window area minimal of $0,75\text{cm}^2$. This is necessary for the easyness of self handwound. Remember that in push-pull system there is 2 primary windings.

(2) $N_s/N_p = V_o/8,8$, where N_s = secondary number of turns, V_o = secondary output voltage

(3) $A_p = 0,004 \times V_o \times I_o$, where A_p = window area of primary wire in mm^2 , V_o = output voltage, I_o = output current.

(4) $A_s = 0,13 \times I_o$, where A_s = window area of secondary wire in mm^2 .

Example : If we use toroidal ferrite core with window area of $A_e = 1 \text{cm}^2$. then from equation no. 1 we will have number of primary turn $N_p = 1,37 \times 10^5 / (50\text{KHz} \times 1 \text{cm}^2) = 2,74$ turns. In practice, number of minimal primary turns is 4 so the primary will cover the whole toroidal core. So we use 4 turns for Q1 and 4 turns for Q2.

From equation (2) we have that $N_s/N_p = 37/8.8 = 4,2$. From here we can calculate that the number of secondary windings is $N_p \times N_p/N_s = 4 \times 4,2 = 16,8$ or 17 windings. Like the primary, in secondary we use 2×17 turns, that is 17 turns for +37V -> 0 and 17 turns for 0-> -37V

Equation (3) is used to determine the number of primary winding wires. We have $A_p = 0,004 \times 74 \times 8 = 2,36\text{mm}^2$. If we use a 1mm diameter magnet wire, we will have window area of $0,785\text{mm}^2$ so we will need 3 wire magnets for each primary windings

Equation (4) is used to determine the number of wire needed for secondary windings. We have $A_s = 0,13 \times 8 = 1\text{mm}^2$ So if we use wire magnet with diameter of 0,8mm(window area = $0,5\text{mm}^2$), then we will need 2 wires with diameter 0,8mm for each secondary windings.

13. The secondary output voltage is rectified by full bridge configuration like in [fig11](#). Bridging diode must be the type of fast rectifier, usually looks like transistor TO220 with plate heatsink. For SMPS we cannot use ordinary 50/60Hz rectifier diode. For this design we use diode type BYW29-150, which have rating of 8A, 150V. We can also use other diodes like with prefixes FE...,MUR..., as long as it is a fast rectifier diode with minimal specification like above.

3. MISCELLANEOUS TIPS FOR MAKING CAR POWER AMPLIFIER

Car power amplifier has specific accessories like preamp gain circuit, an inverting channel so that the power is bridgeable. These functions usually done with opamps. The circuit can be seen in [fig12a](#) and the supply circuit can be seen in [fig12b](#). The circuit is placed before the audio amplifier circuit.

The transformer is handwound on toroidal ferrite core. The output filter inductor can be made with ferrite core material or MPP core material. It can be made with 1.2mm wire magnet, handwound and measured until we have 0,046mH

Handwound the transformer core can be done as follow ([fig13b](#)):

- First we wound the secondary winding of 4 wires of 0.8mm magnet wires at once with 17 numbers of turn. The turn can be made in any direction as long as we consistent with the direction of the wound. If we have finished wounding it, the toroidal core will look like [fig13a](#). We named the wires with wire A, B, C, and D. If we start the wound on top of the core, the end will be at the bottom of the core. Make sure each wire edges with AVOMeter. Connect start edge of wire A and B to point S1 and the end edge of wire A and B to point G. The start edge of wire C and D is connected to point G and the end edge of wire C and D is connected to point S2. Point G will be the secondary ground of the power amplifier and point S1 and S2 will be connected to bridging diode of BYW29.
- After we finished with secondary winding, we start to wound primary winding. Edges of primary wires is placed diagonally to the edges of the secondary wires like in [fig13c](#). Like winding the secondary wires, we wound 6 wires of 1mm diameter at once. Name them wire A, B, C, D, E, and F. Connect the start edge of wire A, B, C to point P1 and the end edge of wire A, B, C to point P+. Connect the start point of wire D, E, F to point P+ and the end edge of wire D, E, F to point P2 ([fig13d](#))

If you have finished winding the primary and the secondary, the whole transformer will have the same wire directions like in [fig12e](#). Connect point P+ to the +12VDC of the car battery, point P1 to the drain of power mosfets Q1 and point P2 to the drain of the power mosfets Q2.

It is important to remember that all tracks in PCB layer that is connected to the power transformer has to have sufficient width due to large current will be involved. Also it is better if we soldered those tracks to have more current transfer.

After finishing winding the transformer, place all the rest of the component and finish assembly of the SMPS. You can test it by connect it with 12VDC input from the battery. Don't forget to connect the remote turn on with 12VDC. There should be output voltage of +37V, 0 and -37V without any large current draw in the 12VDC line. Check for any mistakes, if the output voltage do not present or if the SMPS draws large current from 12VDC input.

In the assembly process of car audio power amplifier, we have to pay attention in mounting all transistors to the heatsink. We must use sufficient heatsink surface so the heat won't damage the amplifier. Use mica isolator and white silicon pasta to make sure the heat transfer. Firmly tighten all the bolts to press all the transistors. Car amplifier works in vigorous environment like in the trunk of a car. Placing an extra fan always a good idea in making car power amplifier.

After we connect the SMPS to the audio amplifier, we are ready to test the car power amplifier. First trim the bias potentiometer fully left side to have minimum bias. Turn on the SMPS and look for the current draw in 12VDC line with ampmeter. The ampmeter indicator will raise for a moment to fill all the capacitors. After a few moment, the ampmeter indicator must turn back to minimum indication of ampere. If not, there is some problem. Then we trim the bias to optimal point. Usually for car stereo power amplifier total quiescent ampere will not exceed 2A of 12VDC line.