

## amp preamplifier

provided by the screen of a screened cable. For proper operation, the screen must be connected to ground, and it cannot be used to carry the signal.
Despite this protection, some interference signals still manage to reach the active conductors. If these conductors have the same impedance relative to ground, the induced signals will also be the same. Their effect can then be neutralized by the differential input stage of the preamplifier. In addition, the low impedance of a dynamic microphone reduces the effect of extemal interference.
In short, use a screened cable with two conductors and solder the cable together as shown in Figure 1.

## Schematic diagram

The schematic diagram consist of two identical amplifier channels. Here we describe one of the two channels. The circuit is powered by a 9-V battery. An LED wired in series indicates that preamplifier is switched on. The volt-

## Features

- Stereo
- Compatible with dynamic and electret microphones
- Maximum input sensitivity: 50,60 or 70 dB , selectable
- Level control using two potentiometers
- Bandwidth: 50 Hz to 50 kHz at maximum gain ( 70 dB )
- Distortion: $\quad 0.04 \% \mathrm{at}-10 \mathrm{dBV}\left(316 \mathrm{mV} \mathrm{V}_{\text {et }}\right)$
$0.12 \%$ at $0 \mathrm{dBV}\left(1 \mathrm{~V}_{\mathrm{EH}}\right)$
- Input noise: $\quad-124 \mathrm{dBV}\left[0.63 \mu \mathrm{~V}_{\mathrm{ef}}\right]$
- Power source: 9-V battery
- Current consumption: 3 mA per channel
- Designed to fit in a commercially available enclosure with a battery compartment.
age drop of the LED (1.6 V to 2 V for a red LED) does not affect the performance of the preamp. The supply voltage is switched via the contacts of the audio socket. In the quiescent state, two contacts prevent T9 and T10 from conducting. The TMOS transistor is thus
cut off, so no voltage is applied to the other components. When a microphone cable is plugged in, the contact in the socket is opened. The supply voltage is now applied to the gate of T9 or T10 via R3 or R33. The TMOS transistor is thus switched on and provides power


Figure 1. Construction of the screened cable link between the microphone and the preamplifiec
to the amplifier channel. The high resistance of R3 and R33 limits the current consumption to $1.6 \mu \mathrm{~A}$ per channel in the 'off' state.

## Amplifier design

Why is it necessary to amplify the signal? The line input of an MP3 player requires a peak signal level of approximately 1 V , which means 2 V peak-topeak. This range is converted to 16 -bit digital values in the device, which thus provides a resolution of $30 \mu \mathrm{~V}$. However, the signal produced by the MD21 at a normal conversation level is only $3.6 \mu \mathrm{~V}$, which is much to low for the analogue-to-digital converter (ADC) of the MP3 player. If you connect the microphone directly to the player, you will make a recording without any sound. For a satisfactory SNR, the level of the
signal applied to the input of the player must be at least 100 times as large as the value of the least significant bit, which means at least 3 mV . The signal from the microphone must be amplified by a factor of 833 to achieve this level. This is the job of the preamplifier.
The preamplifier described here provides a choice of three gains: 315 ( 50 dB ), $1000(60 \mathrm{~dB})$, or $3150(70 \mathrm{~dB})$. Such high gains cannot be obtained in a single stage in combination with an acceptable bandwidth, so this task is split over two stages. The first stage is built using discrete transistors, while the second stage is implemented using an operational amplifier.
In the first stage (shaded grey in Figure 2), you can see the classic structure of a differential transistor amplifier (T1 and T2). The microphone signals arrive via IN1 and IN2, with the capaci-


Figure 2. Full schematic diagram of the microphone preamplifier for MP3 players.
tors providing DC blocking to avoid upsetting the DC bias setting. The output of the first stage is taken across the collectors of T1 and T2.
The gain is determined by the equivalent resistance between the two emitters:
$-2.2 \mathrm{k} \Omega$ : $13.6 \times(23 \mathrm{~dB})$
$-2.2 \mathrm{k} \Omega| | 470 \Omega: 43 \times(33 \mathrm{~dB})$
$-2.2 \mathrm{k} \Omega$ || $33 \Omega: 135 \times(43 \mathrm{~dB})$
Transistors T3 and T4 stabilise the operating point of the stage, which makes it unnecessary to use a matched pair for T1 and T2.

## Why use transistors?

Could be first stage be built using an opamp and a few passive components instead of transistors? The answer is yes with regard to the gain, but no with regard to noise. This can be shown using a simple comparison. We compared the behaviour of two amplifier designs with the same input sensitivity: the transistor stage described above (with S1 set to R12 for a gain of 33 dB ) and an amplifier built using a TL071, which is known for its low noise level. The frequency characteristics are shown in Figure 3. Both circuits meet the requirements, but the transistor stage does it better.
We can use a PSPICE simulation to determine the effective input noise voltage. This calculation takes all noise sources into account. It yields the following results:

- Design using a TL071: noise level $500 \times 10^{-18} \mathrm{~V}^{2} / \mathrm{Hz}$ over the frequency range of 100 Hz to 20 kHz (white noise). This yields
$\mathrm{V}_{\text {efi }}=\sqrt{ }\left[\left(500 \times 10^{-18}\right) \times(20,000)\right]=$ $3.2 \mu \mathrm{~V}$.
- Design ising transistors: oise level $11 . E \sim 1,{ }^{18} \mathrm{~V}^{2} / \mathrm{Hz}$ over the frequency range of 100 Hz to 20 kHz . This yields
$V_{\text {eif }}=\sqrt{ }\left[\left(11.5 \times 10^{-18}\right) \times(20,000)\right]=$ 0.48 uV .

The noise level is thus a factor of 6.6 lower, so the transistor stage wins hands dor-.. This noise level is of the same order as the signal produced by the microphone in a quiet room. This means you can hear a fly buzzing around in the room.
Strictly speaking, you also have to take into account the thermal noise generated by the internal resistance of the microphone. The MD21 has an internal resistance of $200 \Omega$, which yields an effective noise voltage of $8.6 \times 10^{-9} \times \sqrt{R}$

## Examples of acoustic pressures

| Condition | $\mathbf{P}[\mathrm{Pa}]$ | $\mathbf{P}[\mathrm{dBSPL}]$ |
| :--- | :--- | :--- |
| Auditory threshald | $20 \mu$ | 0 |
| Quiet room | $200 \mu$ | 20 |
| Conversation | 2 m | 40 |
| Lively conversation | 20 m | 60 |
| Busy streef | 0.2 | 80 |
| Preumatic harmmer | 2 | 100 |
| Pain threshold | 20 | 120 |

$=0.12 \mu \mathrm{~V}$ (at $25^{\circ} \mathrm{C}$ and a bandwidth of 20 kHz .
Due to the gain of the first stage, an opamp can be used for the second stage with satisfactory results. A TL081 can also be used in place of the TL071 without any appreciable degradation of performance.
The differential structure is maintained to avoid losing 6 dB in input sensitivity. The gain is fixed at $22(27 \mathrm{~dB})$ as determined by resistors R14, R20, R21 and

R22 for the one channel or R42, R43, R36 and R44 for the other channel.
Potentiometers P1 and P2 can be used to independently adjust the output levels as desired. Capacitors C6 and C15 block the DC component to prevent crackling from the potentiometers.

## Construction

All components except the battery are fitted to a printed circuit board. This


Figure 3. Bandwidth of the first stoge. Blue: transistor version. Red: ILO71 version.

## Principall characteristics of a microphone

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Figure 4. Layout of the dooble-sided PCB designed for this project.
is a double-sided, through-hole plated PCB. If you make the board yourself, you will have to make the throughhole connections by hand. The shape of the board is specifically designed to fit an enclosure distributed by Farnell with a compartment for a 9-V battery. We selected PCB-mount chassis con-
nectors for the audio sockets to ensure optimum contact. Note: these are not standard versions.

We advise using a soldering iron with a very fine tip. Start by soldering the SMD parts, since they will difficult to reach later on due to the other compo-
nents. Pay good attention to the polarity of the electrolytic capacitors, which are present in generous numbers on the bottom of the board.
The SMDs are distributed over both sides. Handle the MOS transistors carefully to avoid exposing them to electrostatic charges. Be careful when solder-


LIST
Resistors
$R 1, R 12, R 23, R 34=470 \Omega$
$R 2, R 24=100 \Omega$
$R 3, R 33=4 M \Omega 7$
$R 4, R 5, R 25, R 26=3 \mathrm{k} \Omega 3$
$R 6, R 11, R 27, R 32=6 \mathrm{k} \Omega 8$
$R 7, R 10, R 28, R 31, R 45, R 46=47 \mathrm{k} \Omega$
$R 8, R 9, R 29, R 30=2 \mathrm{k} \Omega$
$R 13, R 35=33 \Omega$
$R 14, R 22, R 36, R 44=220 \mathrm{k} \Omega$
$R 15, R 37=2 \mathrm{k} \Omega 2$
R16-R19,R38-R41 $=22 \Omega$

## $R 20, R 21, R 42, R 43=10 \mathrm{k} \Omega$ <br> P1,P2 = potentiometer $10 \mathrm{k} \Omega, \mathrm{B}$, Alps type RK09K11310KB (Farnell \# 119-1725)

## Capacitors

(all SMD)
C1,C4,C6,C7,C8,C10,C13,C15,C16,C17 , $\mathrm{C} 19-\mathrm{C} 22=10 \mu \mathrm{~F} 16 \mathrm{~V}$ tantalum, Vishay Sprague 595D106X9016B2T (Farnell \# 392-8895)
$\mathrm{C} 2, \mathrm{C} 3, \mathrm{C} 5, \mathrm{C} 9, \mathrm{C} 11, \mathrm{C} 12, \mathrm{C} 14, \mathrm{C} 18=$ $470 \mathrm{nF} / 25 \mathrm{~V}$ tantalum, Vishay Sprague 595D474X9025T2T (Farnell \# 116-6814)

## Semiconductors

D1 $=$ LED, 3 mm , red
T1-T8 = BC856ALT1G, SMD, SOT-23, ON Semiconductor (Farnell \#114-7782)

T9, $110=2$ N7002, MOSFET, SMD, SOIC
Texas Instruments (Farnell \#102-1754)
$I C 1, I C 2=$ TL071CD, SMD, SOIC, Texas Instruments (Farnell \# 958-9449)

## Miscellaneous

$\mathrm{K} 1, \mathrm{~K} 2, \mathrm{~K} 3=3.5 \mathrm{~mm}$ jack socket with 3 contacts, Schurter R36310000 (Farnell \# 149-933)
S1,S2 = SPST switch, angled pins, PCB mount, height $=12.7 \mathrm{~mm}$, C\&K 7103MD9 AV2BE (Farnell \# 957-5510)
$\mathrm{BT} 1=9 \mathrm{~V}$ battery with clip-on lead $K 4=2$-way PCB pinheader
Case with baffery compartment, e.g. BC2, Farnell \# 223-554
PCB, ref. 060237-I from ThePCBShop
ing the resistors for switches S1 and S2 (R12, R13, R15, R34, R35, and R37): solder only the ends of these resistors that are not connected to the corresponding switches. The other ends will be soldered when you fit the switches to the board. If you solder them before you fit the switches, the holes may be filled with solder.

Be sure to do a neat job of soldering, since many of the solder pads are close together. If you etch your own PCB, be sure to make the through connections between the top and bottom sides carefully and avoid making any shorts, which would be difficult to find later on.

## Enclosure

Once the circuit board is finished and you have checked that it works properly, you can fit it in the enclosure with the battery compartment. Make holes in the bottom part of the enclosure for the input and output connectors and the two switches. The top part must have holes for the two potentiometers and the LED, which adds a bit of flair to the top of the enclosure (a square or rectangular LED is a good choice here, with the leads trimmed to the right length).

## Pulting it to use

After you're satisfied that the preamplifier is working properly, you can start using it. All you have to do is to connect two microphones to the input connectors (K1 and K2) and connect the output to the line input of your MP3 player, and you're ready to go. Use a length of screened stereo cable for the connection to the MP3 player.
Here's to good recordings!
(080c34.4)


## Measured resulits

Due to the very low input levels and the fact that it was not possible to produce the necessary levels directly using the available signal generators, we made an attenuator cable as shown in Figure 5.


Characteristics:
Attenuation: 2000 ( 66 dB )

Oufput impedance: $680 \Omega$
(nearly the same as a dynamic microphone) Preamplifier operafing in differential mode

Figure 5.
Electitical diagram of the ottenvator coble.

## Results

The three curves correspond to the three settings of switch S1.
Measured results:
Setting 1: Maximum gain $=1 \mathrm{~dB}+66 \mathrm{~dB}=67 \mathrm{~dB}$. This is nearly the design value of 70 dB . Lower - 3 -dB point: 50 Hz

Setting 2: Moximum gain $=-8 \mathrm{~dB}+66 \mathrm{~dB}=58 \mathrm{~dB}$. This is nearly the design value of 60 dB . Lower -3 - dB point: 50 Hz

Setting 3: Maximum gain $=-18 d B+66 d B=48 d B$. This is nearly the design value of $50 d B$. Lower -3 dB point: 50 Hz

The upper -3 dB point is above $100 \mathrm{kHz}(-2 \mathrm{~dB}$ at 100 kHz$)$.

Noise and distortion
The noise and distortion figures were measured by the author. The results we obtained with our own analyser (Audio Precision) are nearly the same.

Results

| Silidist | $\begin{aligned} & 5_{\text {Bldiv] }} \\ & \text { Clilktz } \end{aligned}$ | $\frac{5}{[10]}$ | Mempred goin | SIIN | IHD | Outpul moiselenel | Input noiselonel |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Goin max | -1 | 0 | 67 dB | 57 dB | 0.12\% | -57 d8 | $-124 \mathrm{dBV}$ | $0.63 \mu V_{47}$ |
| Goin mojen | +8 | 0 | 58 dB | 65 dB | 0.12\% | -65 dB | $-123 \mathrm{dBV}$ | $0.71 \mu \nu_{\text {en }}$ |
| Goin minl | +18 | 0 | 48 dB | 72 dB | 0.12\% | -72dB | $-120 \mathrm{dBV}$ |  |

$\begin{array}{ll}\text { Distorsion } & 0.12 \% \text { of } V_{\text {out }}=0 \mathrm{dBV} \\ & 0.04 \% \text { of } V_{\text {out }}=10 \mathrm{dBV}\end{array}$


Figure 6.
The resulls measured by the outhor are very close to our meosured results.

## Corrections \& Updates

## MP3 Preamp

February 2007, p. 40-45, 060237-I
On the PCB component overlay, the labels of SMD resistors R29 and R32 have been transposed. Resistor $29(2 \mathrm{k} \Omega)$ should be the top device in the row of resistors fitted to the right of S1 and S2. R2 ( $6 \mathrm{k} \Omega 8$ ) should be directly below it.

Ethermeter
March 2007, p. 72-74, 075035-I Due to a crashed hard disk in the author's PC an early version of the circuit diagram was printed. The correct schematic is reproduced here.

## Canon EOS Cameras go

Wireless
July/August 2004, p. 102, 030432-1.
In the transmitter circuit diagram, pushbutton S 1 should be a normally closed (NC) type.


4/2007 - elektor electronics


[^0]:    - Sensitivity in $\mathrm{mV} / \mathrm{Pa}$
    - Output impedance
    - Bandwidth
    - Directianal sensitivity
    - Maximum acoustic pressure

    An electronics specialist is interested in the first three characteristics, while a recording specialist is interested in the last three.

    The signal voltage provided by a microphone is proportional to the acoustic pressure and the sensitivity of the microphone:

    - $V_{\text {mC }}=S \times P$
    - S : sensifivity in $\mathrm{V} / \mathrm{Pa}$
    - P: acoustic pressure deviation in Pa

