

## A 100-Watt, 18-kHz Inverter Using RCA-2N5202 Silicon Power Transistors

by

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This Note describes a two-transistor, two-transformer inverter that demonstrates the excellent switching capabilities of the new RCA-2N5202 power transistor. This silicon epitaxial n-p-n device is supplied in the popular TO-66 package. Its fast switching speed makes it especially suitable for use in switching regulators, switching control amplifiers, converters, and inverters. Pertinent characteristics of the 2N5202 are shown in Table I.

Fig.1 shows a schematic diagram of the two-transistor, two-transformer circuit. A saturable base-drive transformer  $T_2$  controls the inverter switching operation. A linearly operating output transformer  $T_1$  transfers the output power to the load. The output transformer  $T_1$  is not allowed to saturate; therefore, the peak collector current through the transistor is determined principally by the value of the load impedance.

Because no two transistors are perfectly matched, one of the transistors in the inverter circuit conducts more rapidly than the other when the power is turned on. This transistor,  $Q_2$  for example, tends toward saturation and causes positive voltages to appear at the dotted ends of the transformers. Thus, there is an effective positive feedback that causes  $Q_1$  to switch off and  $Q_2$  to switch on. The voltage from the collector of  $Q_1$  to the collector of  $Q_2$  is then positive and equal to twice the collector supply voltage  $V_{CC}$ . The voltage  $V_{Rfb}$  across the feedback resistor  $R_{fb}$  is essentially the product of the resistance  $R_{fb}$  and the base current referred to the primary of  $T_2$ . The voltage across  $T_2$  is equal to  $2 V_{CC} - V_{Rfb}$ .

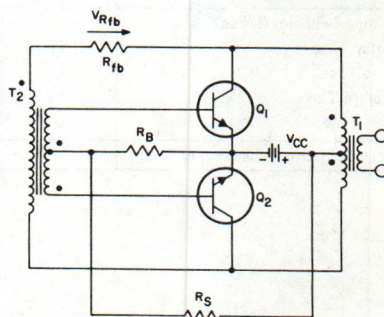


Fig.1 - Schematic diagram of two-transistor/two-transformer inverter.

At the beginning of the next half-cycle, the voltage across  $R_{fb}$  increases very slowly with the slowly increasing magnetizing current through  $T_2$ . When  $T_2$  reaches its saturation flux density, the magnetizing current increases very rapidly and causes a rapid increase in  $V_{Rfb}$ . As a result, the voltage across  $T_2$  decreases rapidly and  $Q_2$  comes out of saturation. The collector voltage of  $Q_2$  then rises, and regenerative action causes  $Q_1$  and  $Q_2$  to reverse states. As these processes are repeated during succeeding half-cycles, oscillations are sustained.

Characteristics of the drive transformer and the output transformer used in the circuit of Fig.1 are de-

TABLE I - TYPICAL CHARACTERISTICS OF RCA-2N5202 SILICON POWER TRANSISTOR

CHARACTERISTICS	SYMBOLS	TEST CONDITIONS	MIN	MAX	UNITS
Collector-Cutoff Current	$I_{CEV}$	$V_{CE} = 100 \text{ V}, V_{BE} = -1.5 \text{ V}$	-	10	mA
		$V_{CE} = 100 \text{ V}, V_{BE} = -1.5 \text{ V}, T_C = 150^\circ\text{C}$	-	10	mA
Emitter-Cutoff Current	$I_{EBO}$	$V_{EB} = 6 \text{ V}, I_C = 0$	-	10	mA
DC Forward-Current Transfer Ratio	$h_{FE}$	$V_{CE} = 1.2 \text{ V}, I_C = 4 \text{ A}$	10	100	
Collector-to-Emitter Sustaining Voltage	$V_{CE(sus)}$	$R_{BE} = 50 \Omega, I_C = 0.2 \text{ A}$	75	-	V
Base-to-Emitter Voltage	$V_{BE}$	$V_{CE} = 1.2 \text{ V}, I_C = 4 \text{ A}$	-	1.9	V
Collector-to-Emitter Saturation Voltage	$V_{CE(sat)}$	$I_C = 4 \text{ A}, I_B = 0.4 \text{ A}$	-	1.2	V
Small-Signal Forward-Current Transfer Ratio	$h_{fe}$	$V_{CE} = 10 \text{ V}, I_C = 0.5 \text{ A}, f = 10 \text{ MHz}$	6	-	
Output Capacitance	$C_{ob}$	$V_{CB} = 10 \text{ V}, I_E = 0, f = 1 \text{ MHz}$	-	175	pF
Second-Breakdown Collector Current	$I_{S/b}$	$V_{CE} = 40 \text{ V}$ (base forward-biased)	400	-	mA
Second-Breakdown Energy	$E_{S/b}$	$V_{BB} = -4 \text{ V}, R_{BE} = 50 \Omega, L = 50 \mu\text{H}$	0.4	-	mJ
Saturating Switching Times:					
Delay Time	$t_d$	$V_{CC} = 30 \text{ V}, I_C = 4 \text{ A}, I_{B1} = 0.4 \text{ A}$	-	40	ns
Rise Time	$t_r$	$V_{CC} = 30 \text{ V}, I_C = 4 \text{ A}, I_{B1} = 0.4 \text{ A}$	-	400	ns
Storage Time	$t_s$	$V_{CC} = 30 \text{ V}, I_C = 4 \text{ A}, I_{B1} = 0.4 \text{ A}, I_{B2} = -0.4 \text{ A}$	-	800	ns
Fall Time	$t_f$	$V_{CC} = 30 \text{ V}, I_C = 4 \text{ A}, I_{B1} = 0.4 \text{ A}, I_{B2} = -0.4 \text{ A}$	-	400	ns
Thermal Resistance, Junction to Case	$\theta_{J-C}$		-	5	$^\circ\text{C/W}$

terminated by means of the following equation:

$$N_p = \frac{V}{4fAB} \times 10^8$$

where  $N_p$  is the number of turns in the primary winding,  $V$  is the peak voltage across the primary winding,  $f$  is the operating frequency in hertz,  $A$  is the cross-sectional area of the core in square centimeters, and  $B$  is the flux density in gauss. In the design of the drive transformer  $T_2$ , the value of flux density  $B$  is selected to cause the core to saturate. For the output transformer  $T_1$ , the value of  $B$  is selected to assure that  $T_1$  will not saturate. The base resistor  $R_B$  is determined by the voltage at the secondary of  $T_2$  and the base drive required for the transistor. The resistor  $R_S$  is selected so that a voltage of 0.7 volt appears across  $R_B$  when the power is turned on initially.\*

\* A complete discussion of inverter design considerations and design information is given in RCA Application Note SMA-37: "High-Speed Inverters Using Silicon Power Transistors" by H.T. Breece.

Fig.2 shows the circuit diagram for a practical 100-watt, 18-kHz inverter using RCA-2N5202 transistors. Performance characteristics for this inverter are shown in Fig.3, and waveforms of output voltage, collector voltage, and collector current as functions of time are shown in Fig.4.

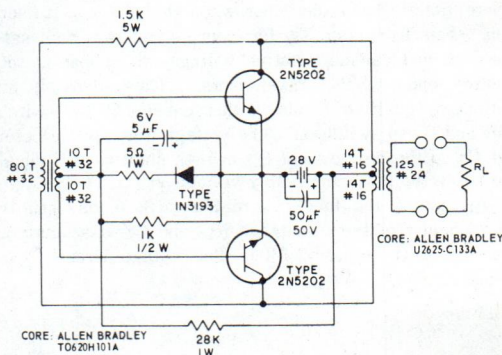


Fig.2 - Circuit diagram for 100-watt, 18-kHz inverter.

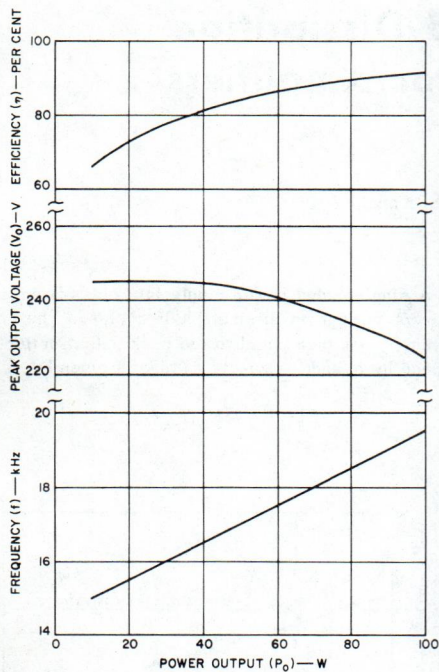


Fig.3 - Performance characteristics of inverter shown in Fig.2.

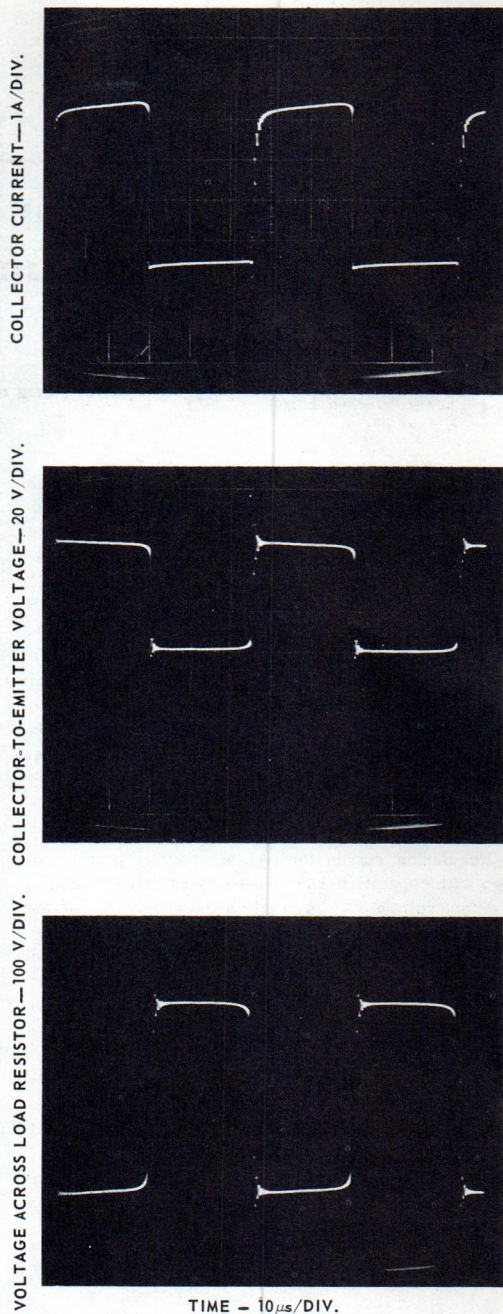


Fig.4 - Waveforms of output voltage, collector voltage, and collector current in inverter of Fig.2.